

WATER HEATING ENERGY USE REDUCTIONS FROM EPA WATERSENSE LAVATORY PLUMBING FITTINGS

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1 **ABSTRACT**

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3 Hot water savings from water-efficient lavatory fittings lead to reductions in water heating energy
4 consumption, and ultimately to decreases in carbon emissions. This paper characterizes existing
5 and proposed approaches used to estimate hot water savings and carbon emissions reductions
6 stemming from the U.S. Environmental Protection Agency’s WaterSense program. Also described
7 are refinements that improve the accuracy of residential hot water use percentage estimates of
8 lavatory fittings. The authors conclude that (1) hot water percentages for showers and faucets
9 calculated using up-to-date, publicly available national data are consistent with those found by
10 regional studies and household-level models of water use; (2) the accuracy of heating energy
11 savings estimates attributable to WaterSense-labeled lavatory products, as well as associated
12 emissions reductions, can be refined by modifying the existing energy factor/uniform energy factor
13 (EF/UEF)-based estimation approach with available data. The refined approach accounts for more
14 nuanced conditions than the EF/UEF-based approach but depends on data not always available;
15 and (3) the approaches described and intermediate outputs can be generalized for other water
16 conservation programs or estimating purposes.

17 **Keywords:** Hot water, Residential water use, WaterSense, Water conservation, Water heating

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19 Word count: 6763
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21
22

1 INTRODUCTION

23 All water contains energy that is used to extract, transport, treat, and deliver both potable
24 water and wastewater. A 2013 report from the Electric Power Research Institute (EPRI) found that
25 U.S. public drinking water systems consumed roughly 39.2 billion kWh for this purpose, while
26 municipal wastewater treatment systems consumed 30.2 billion kWh per year. These uses
27 combined represent roughly 2 percent of the total electricity use in the U.S. annually (EPRI, 2013)
28 and can be as much as 13 percent of total U.S. annual electricity use with water end uses included
29 (Griffiths-Sattenspiel and Wilson, 2009). What is more, higher energy intensity sources and
30 treatment strategies (such as desalination or reclaiming wastewater for new purposes) currently
31 represent small but growing portions of the overall treatment profiles. The trends indicate that
32 these values will rise both nominally from increases in population and development, and
33 proportionally from increased use of high intensity sources and treatment (EPRI, 2013).

34 Hot water-using fittings and appliances can have additional energy consumption at the
35 point of use in the form of hot water; resulting in a substantial economic impact on consumers with
36 U.S. households spending an average of \$300 USD annually on energy to heat water (U.S. EIA,
37 2015a). Consumers typically use hot water from a range of water-using appliances and fittings,
38 including those found in the kitchen, lavatory, and laundry room.

39 The amount of energy embedded in water from transport, treatment, and heating, along
40 with the volume of water needed to support thermoelectric cooling during power generation
41 (Dieter *et al.*, 2018), have driven an increased focus on the connection between water and energy
42 in recent years. It has also led to increased interest in reducing hot water use as a strategy for
43 energy savings. An analysis found that showerheads and faucets (taps for both kitchen and
44 lavatories) could save a cumulative total of 63.6 and 60.3 million metric tons of CO₂ through the

45 year 2050 from reductions in water heating loads.¹ This ranks faucets and showerheads fifth and
46 sixth highest in potential carbon savings among the 27 different appliance/end uses assessed,
47 placing a larger potential carbon savings on showerheads and faucets than on traditional energy
48 efficiency targets such as air conditioners, refrigerators, and freezers (ACEEE, 2020).

49 The desire to maximize energy and carbon savings has driven an increase in interest in
50 capturing the relationship between water and energy, and the energy savings that water efficiency
51 may offer. One such use case that can provide helpful data to others facing similar goals for
52 quantification is the U.S. Environmental Protection Agency (EPA)'s voluntary WaterSense
53 program. EPA estimates savings associated with labeled water-efficient fittings (as well as other
54 products) that have been third-party certified to meet both the efficiency and performance
55 requirements of WaterSense specifications. Current WaterSense-labeled residential products that
56 use hot water are showerheads and lavatory faucets (also called lavatory fittings or taps). As hot
57 water use is reduced, energy savings increase and carbon emissions are further lowered.

58 Reductions in the amount of hot water used by water-using fittings and appliances can be
59 expressed as gallons, as energy (kWh or kJ), as financial impacts quantified from consumer water
60 and energy bills, and as greenhouse gas emission impacts quantified as carbon by applying EPA
61 carbon dioxide multipliers. A full and accurate accounting of the program's impact on water and
62 energy use, and associated carbon savings, is considered vital to properly monitor the success of
63 the program and report its impacts. This requires the considered selection of inputs. Several
64 publicly available datasets include some of these inputs, while others must be modeled or estimated
65 from best available data. Data points that the authors were not able to find in publicly available

¹ These numbers are based solely on water heating load reductions and exclude the embedded energy and associated carbon savings that are realized from reduced extraction, treatment, and conveyance. The actual savings could be even higher.

66 datasets and had to be modeled from other source data are discussed in this paper. The authors
67 recognize that water-using products and consumer water use may vary significantly between
68 countries. However, given the paper's focus on the water and energy savings assessment of U.S.
69 EPA's WaterSense program, the studies cited and conclusions made are specific to the United
70 States as a study sample of the methods discussed. Additionally, unlike other countries, the United
71 States has no regular national survey or accounting of water demand by end use. Due to the lack
72 of water-specific national surveys and regularly conducted field metering studies in the United
73 States, authors employed existing studies and considered data availability limitations in developing
74 their approach.

75 The WaterSense program employs several analytical models to estimate the change in
76 water use attributable to the improved efficiency of labeled products (Schein *et al.*, 2019). This
77 paper focuses on several refinements to inputs used in these analytical models needed to accurately
78 estimate the total energy and carbon savings associated with the demonstrated water use savings.
79 It explores existing and proposed methods of (1) creating a nationally representative picture of the
80 likely mix of hot and cold water in residential plumbing fittings at the point of use, (2) establishing
81 the heating energy savings associated with hot water savings from more efficient fittings, and (3)
82 calculating resulting carbon emission reductions. Section 2 of this paper summarizes the approach
83 used to estimate the hot water percentage of lavatory fitting total water consumption that
84 incorporates geographical temperature differences into the calculation of hot water saved by the
85 WaterSense program (or water use savings in general). Section 3 describes two approaches for
86 estimating total hot water energy savings from the WaterSense program, one using water heater
87 energy factors/uniform energy factors (EF/UEF) and the other employing the Water Heater
88 Analysis Model (WHAM), and compares results. The authors conclude that the latter is the

89 preferred method, but that currently available data on water heating technology limits its use at
90 scale. Section 4 describes the approach for determining associated carbon emission reduction
91 estimates, and Section 5 discusses results before proposing future possibilities for model
92 amendments.

93 **2 LAVATORY FITTING HOT WATER PERCENTAGE AND USE**

94 EPA regularly evaluates its WaterSense program impacts using models that require readily
95 available, nationally representative data. Approximations and assumptions must be made to
96 available data because actual household water use data are not regularly gathered, are not apt to be
97 nationally representative, and may not include critical model inputs. The authors propose an
98 approach that employs nationally representative data from the Energy Information Administration
99 (EIA) and Housing and Urban Development (HUD) to improve the accuracy of evaluating the hot
100 water percentage used in lavatory fittings over time.

101 **2.1 Field data for hot/cold water mix values**

102 The percentage of hot water used by lavatory fittings is crucial in determining heating
103 energy savings associated with more efficient fittings. In the absence of data from direct
104 measurement and metering of hot water consumption in a representative sample of households,
105 this percentage has conventionally been estimated using point values from publicly available
106 studies. For the last 20 years, residential hot water use has been disaggregated into end uses. Prior
107 to 2000, hot water usage studies for Canada and the United States reported total residential hot
108 water for medium to small numbers of homes in limited geographic areas (Perlman and Mills,
109 1985; Merrigan, 1988; Becker and Stogsdill, 1990; Abrams and Shedd, 1996). In the late 1990s,
110 residential studies disaggregated hot water end use using a variety of approaches: attaching
111 thermocouples onto hot water pipes and conducting flow-trace analyses according to “flow

112 signatures” (Lowenstein and Hiller, 1998; DeOreo and Mayer, 2000). More recent figures on hot
113 water use suggest the effects of a decrease in household members and an increase in water-efficient
114 fittings (Hendron *et al.*, 2010; Evarts and Swan, 2013; Parker *et al.*, 2015; Escriva-Bou *et al.* 2015).
115 See Chen *et al.* (2020) for more discussion of these studies.

116 Available field data on hot/cold water mix values are sparse. The percent of overall water
117 use that is hot water at various fittings was determined via flow-trace analysis in 10 single-family
118 homes in Seattle (DeOreo and Mayer, 2000); in 20 representative single-family homes in Seattle
119 and the San Francisco Bay Area before and after a retrofit with high-efficiency products
120 (Aquacraft, 2005); and in 94 residences in nine North American locations (DeOreo *et al.*, 2016).
121 Table 3 displays these percentages (section 2.4.2). Alternatively, hot water use in residential
122 buildings varies according to a number of factors: regional climate (which impacts inlet water
123 temperature), water heater setpoint temperature, hot water flow piping configurations from the
124 water heater equipment, installed fittings and appliances, household occupancy numbers, occupant
125 behavior, and household occupant ages (Evarts and Swan, 2013).

126 Previously, WaterSense models used the point value of 72 percent for hot water percentage
127 for lavatory fittings (Aquacraft, 2005). The rest of this section describes the refined method now
128 used in the WaterSense models to estimate lavatory fitting hot water percentages.

129 **2.2 Determining lavatory fitting hot water use using ANSI-301**

130 The American National Standards Institute (ANSI) 301 standard (ANSI 301-2019) was
131 developed under the Residential Energy Services Network (RESNET) with the goal of providing
132 a “consistent, uniform methodology for evaluating and labeling the energy performance of
133 residences.” First published in 2014, the first 301 standard, *ANSI/RESNET/ICC 301-2014*,
134 *Standard for the Calculation and Labeling of the Energy Performance of Low-rise Residential*

135 *Buildings using an Energy Rating Index*, has been amended to include an approach to estimate
136 daily hot water use volumes.

137 The ANSI-301 hot water draw model, referenced as Equation 4.2-2 in *ANSI/RESNET/ICC*
138 *301-2014*, is used in this paper; it permits comparable hot water use estimates for the end uses of
139 interest, lavatory faucets and showerheads, while including related hot water waste. The ANSI-
140 301 model established a method to assess daily hot water gallon use through dishwasher and
141 clothes washer use, a number of climatic conditions, and dwelling characteristics thought to have
142 implications on household size, among other factors. The equation and inputs are shown below.

$$143 \quad HW_{gpd} = (refDW_{gpd} + refCW_{gpd} + F_{mix} \times (refF_{gpd} + refW_{gpd})) \quad \text{Equation 1}$$

145
146 Where:

147 HW_{gpd} = gallons per day of hot water use,

148 $refDW_{gpd}$ = reference dishwasher gallons per day,

149 = $(0.7801 \times Nbr) + 1.976$,

150 Nbr = number of bedrooms in the rated home, not to be less than 1,

151 $refCW_{gpd}$ = reference clothes washer gallons per day

152 = $(0.6762 \times Nbr) + 2.3847$,

153 F_{mix} = $1 - \frac{(T_{setTemp} - T_{mix})}{(T_{setTemp} - T_{inletTemp})}$; see Section 2.4.1 for description of these

154 temperatures,

155 $refF_{gpd}$ = reference climate-normalized daily fixture water use in Energy Rating

156 Reference Home (in gallons per day)

157 = $14.6 + 10.0 \times Nbr$, and

158 $refW_{gpd}$ = reference climate-normalized daily hot water waste due to distribution system

159 losses in Energy Rating Reference Home (in gallons per day)

160
$$= 9.8 \times Nbr^{0.43}.$$

161 Employing ANSI-301 allows estimates of hot water use to approximate occupancy
162 differences without requiring data on operational characteristics and demography. Using readily
163 available national representative data allows WaterSense program estimates to remain current as
164 both water use trends and the make-up of the housing stock continue to change over time.

165 **2.3 Determination of inputs**

166 This section summarizes the inputs used to estimate hot water use and percentage of hot
167 water per unit volume of water.

168 *2.3.1 Regional differences and bedroom number*

169 ANSI 301-2019 relies on publicly available data of number of bedroom counts by housing
170 unit vintage (American National Standards Institute, 2014) instead of data on household age
171 groups or number of occupants, which may not be consistently available. Two studies assert that
172 the amount of residential hot water use correlates to the number of household members (Parker *et*
173 *al.*, 2015; Lutz, 2005). Parker *et al.* (2015) demonstrated that even though home occupant age and
174 number are better predictors of hot water use in individual homes, a reasonable substitute is the
175 home's bedroom count.

176 The ANSI 301-2019 method using the home's bedroom count as an indicator of household
177 occupancy allows for estimation of hot water use when other household characteristics are not
178 available (as is the case for home energy ratings and building code calculations). Using EIA's
179 Residential Energy Consumption Survey (RECS 2015) data as the input for number of bedrooms
180 allows regional adjustments to total household water use and hot water use by appliance or fitting
181 with improved accuracy (U.S. EIA, 2015a). Because ANSI 301-2019 uses number of bedrooms to
182 approximate household size (number of occupants), the authors examined the relationship between
183 household size and number of bedrooms using several nationally representative datasets; see

184 American National Standards Institute (2019) and Chen *et al.* (2020) for more detail. The authors
185 find that with a robust sample size, both RECS 2015 and HUD’s American Housing Survey (AHS
186 2017) data show a strong linear and positive correlation between the numbers of bedrooms and
187 household size for single-family homes, with little variability (U.S. HUD, 2017). Based on this
188 analysis, the authors conclude that the number of bedrooms is a reasonable proxy for household
189 size.

190 2.3.2 *Water heater setpoint temperature*

191 In the field, the water heater setpoint temperature ($T_{setTemp}$) varies by household, but to the
192 authors’ knowledge, apart from a regional study of 127 homes with electric resistance water
193 heaters in Central Florida (Parker, 2002) showing that audited setpoint temperature averaged
194 52.8°C and field measurement studies in California (Lutz, 2012) showing an average setpoint
195 temperature of 50.6°C, no national household dataset reporting setpoint temperatures exists.
196 Therefore, instead the authors use 51.7 °C (125°F) based on ANSI 301-2019 (ANSI, 2019) for tank
197 setpoint temperature. It is worth noting that the tank setpoint temperatures do not necessarily match
198 outlet water temperatures or account for temperature drift within a storage water heater, but are
199 used here as the best available proxy.

200 2.3.3 *Inlet water temperature*

201 Water inlet temperature influences the energy impact of hot water-using plumbing fittings
202 both by affecting the required temperature rise to the water heater setpoint and by influencing the
203 temperature of cold side premise plumbing. Colder temperature in the cold water lines can result
204 in a higher percent mix to achieve the user-desired warm water temperature.

205 Inlet water temperature can be estimated from either air or groundwater temperature as
206 prior studies have shown. An ANSI 301-2019 equation calculating cold water inlet temperatures

207 was first referenced by Hendron *et al.* (2004) and is based on Burch and Christensen (2007). The
 208 ANSI 301-2019 equation for cold water inlet temperature is lengthy and not repeated here for
 209 space considerations (ANSI, 2019) but can be simplified by using the annual average outdoor
 210 temperature ($T_{airTemp}$) plus 3.3°C (6°F) offset, assuming that the ground water temperature is
 211 slightly warmer than air temperature.

212 Using the relationship between the annual average groundwater temperature and the annual
 213 average outdoor air temperature based on Yoshitake *et al.* (2002), which reports the relationship
 214 between groundwater temperature and annual average temperature, the resulting equation is:

$$215 \quad T_{inletTemp}^{°F} = T_{airTemp}^{°F} + 6 \text{ °F} = \frac{(T_{gwt}^{°F} - 12.1)}{0.83} + 6 \text{ °F}$$

$$216 \quad T_{inletTemp}^{°C} = T_{airTemp}^{°C} + 3.33 \text{ °C} = \frac{(T_{gwt}^{°C} + 11.06)}{0.83} - 14.44$$

217 **Equation 2**

218 Where:

- 219 $T_{inletTemp}$ = water inlet temperature,
- 220 $T_{airTemp}$ = annual average outdoor air temperature,
- 221 T_{gwt} = average annual ground water temperature.

222 Groundwater temperatures vary over geographic areas, as do cold water inlet temperatures
 223 (see Table 1). The previous estimate for temperature delta (water heater minus cold water inlet)
 224 used by EPA’s WaterSense program was 41.7°C (75.0°F). The results of the analysis presented
 225 here support employing a temperature delta value of 35.8°C (64.5°F), calculated via subtracting
 226 the weighted average of cold water inlet temperature across Census divisions using the RECS 2015
 227 data of 15.8°C (60.5°F) (see section 2.4.1 for more details) from the water heater setpoint
 228 temperature of 51.7°C (125.0°F).

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Table 1: Distribution of Hot Water Use Percentages by Census Division Calculated from RECS 2015 Data and Study Comparisons (*proposed values bolded*)

Census Division	Population	Groundwater temperature from RECS 2015 (°C, °F)	Inlet water temperature (°C, °F)	Hot water percentage for showerheads	Hot water percentage for lavatory faucets
1	5,628,844	8.2, 46.8	8.8, 47.8	74.0	66.2
2	15,377,694	9.9, 49.8	10.8, 51.4	72.7	65.0
3	18,094,391	9.6, 49.2	10.4, 50.7	73.0	65.3
4	8,277,344	10.3, 50.6	11.3, 52.4	72.3	64.7
5	23,474,851	18.2, 64.7	20.8, 69.4	62.6	56.0
6	7,197,189	16.6, 61.9	18.9, 66.0	65.6	58.7
7	13,769,934	19.9, 67.9	22.9, 73.2	61.0	54.6
8 (North)	4,246,877	8.0, 46.4	8.5, 47.3	74.2	66.3
8 (South)	4,266,870	17.6, 63.6	20.1, 68.1	64.1	57.3
9	17,874,256	15.6, 60.1	17.7, 63.8	66.7	59.6
Weighted average		14.1, 57.4	15.8, 60.5	67.8	60.7
Aquacraft (2005)^a				72.0	72.0
DeOreo <i>et al.</i> (2016)^b				66.2	57.0

232 ^a Values are from post-retrofit stage of the study, and faucets encompassed all faucets, not only lavatory faucets.

233 ^b Faucets in this study encompassed all faucets, not only lavatory faucets.

234
235

236 *2.3.4 Temperature mix for shower and lavatory faucet use*

237 Based on ANSI-301, warm water temperatures (T_{mix}) for showers are 40.6°C (105°F).
 238 Faucet hot water use is adjusted given that people use faucet hot water differently from showerhead
 239 hot water (*e.g.*, faucet hot water may be mixed into cold water when people shave or face wash
 240 but not during hand washing or teeth brushing.) The authors assumed that faucet use includes hot
 241 water for 89.4 percent of overall use based on the average ratio of hot water use by faucets and
 242 showerheads weighted by number of sample households in field studies. ²

² DeOreo et al. (2000) showed a ratio of 0.995; Aquacraft (2005) had a ratio of 1; and DeOreo et al. (2016) showed a ratio of 0.861. Note that these studies looked at all indoor faucets (were not limited to lavatory faucets).

243 **2.4 Results**

244 This section shows results using the inputs determined in section 2.3 for determining the
245 percentage of lavatory fitting use that constitutes hot water and for estimating the amount of hot
246 water used by lavatory fittings.

247 *2.4.1 Hot water percentages for lavatory fitting use*

248 Hot water percentages for showerheads and lavatory faucets (F_{mix}) are calculated using
249 water heater setpoint, water inlet, and temperature mix (fitting/user target temperature) and assume
250 no volumetric measurement, which can be interpreted as the assumption that consumers may not
251 wait for the water to come up to a desired temperature. See Equation 3 based on ANSI 301-2019.
252 The temperature for the water heater setpoint is assumed to be 51.7°C (125°F), explained in Section
253 2.3.2. Adjusted RECS 2015 household data are used for cold water inlet temperature. The
254 temperature for showerheads and faucets is represented by T_{mix} , 40.6°C (105°F).

255
$$F_{mix} = 1 - \frac{(T_{setTemp} - T_{mix})}{(T_{setTemp} - T_{inletTemp})}$$
 Equation 3

256 Where:

257 F_{mix} = percentage of hot water for shower event and lavatory faucet usage,

258 $T_{setTemp}$ = water heater setpoint temperature,

259 T_{mix} = fitting/user target temperature.

260 .

261 Table 1 shows showerhead and faucet hot water percentages by Census Division, with
262 findings from other studies included for comparison. The hot water by end use estimation includes
263 the percentages given in Table 1.

264 2.4.2 Average hot water use volume per day for lavatory fittings

265 Hot water from a water heater may be used intentionally by a consumer (e.g., by taking a
 266 hot shower), or unintentionally, as hot water may not always reach the end-use in time to be used
 267 by the consumer. (The water waste volume can be as much as 25 percent of hot water use according
 268 to ANSI 301-2019.)

269 Three assumptions were made for the intentional hot water use estimation: (1) no hot water
 270 use for hand-washing clothes for households without clothes washers, (2) no hot water use in the
 271 dish pre-washing step for older dishwasher models, and (3) faucet and showerhead flow rates are
 272 at the federal standard, noting that this value will fluctuate across households. See Table 2.

273 **Table 2: Inputs for Lavatory Fitting Use Calculations**

Input	Kitchen faucets	Lavatory faucets	Showerheads
Minutes per person per day	5 ^a	3 ^a	5 ^a
Liters per minute (U.S. Gallons per minute)	8.3 (2.2 ^b)	8.3 (2.2 ^b)	9.5 (2.5 ^b)

275 ^a Baumann *et al.* (1998)

276 ^b Energy Policy Act (1992), Federal Standard from EPACKT 1992

277 <https://www.govinfo.gov/content/pkg/CHRG-106hhrg58509/html/CHRG-106hhrg58509.htm>

278

279 The ANSI 301-2019 equation gathers together all fitting hot water use. The authors
 280 distinguished different fitting hot water use percentages using the average minutes of use for each
 281 fitting type. For the showerhead hot water percentage, total fitting hot water volume is multiplied
 282 by the ratio of shower use in minutes over all fitting use in minutes. On average, shower use is
 283 assumed to be 88 percent of total shower and bath water use, based on DeOreo *et al.* (2016). For
 284 faucet use between kitchens and lavatories, a ratio of minutes for each fitting type is multiplied by
 285 total fitting hot water volume. Table 3 compares the estimated hot water use percentage developed
 286 in this study to those from selected studies.

287

288

Table 3: Estimates of Percentage of Showerhead and Faucet Hot Water Use

	Lowenstein and Hiller (1998)	DeOreo and Mayer (2000)	Escriva-Bou <i>et al.</i> (2015)	DeOreo <i>et al.</i> (2016)	Using ANSI 301-2019 and RECS 2015 Data
Location	Unspecified	WA	CA	AZ, CO, FL GA, ON, TX, and WA	National
Sample size	14	10	>700	94	5,686
Percent of total residential hot water use, by end use (%)					
Showers	41.6	25.1	41	39.1	34.8
Faucets	Kitchen				27.5
	Lavatory	--	34.3	39	33.8

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3 DETERMINATION OF LAVATORY FITTING ENERGY SAVINGS

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More water-efficient showerheads and lavatory faucets also save energy from a reduction

292

in the hot water used. One approach to calculate the amount of energy saved from a hot water

293

usage reduction can employ a time series of annual stock-weighted EF and UEF for both electric

294

and gas water heaters; the stock of water heaters obtained based on the combination of shipments

295

and the survival function; time series of annual water savings; the percentage of houses using gas

296

or electric for water heating; and the percentage of hot water used by lavatory fittings. A second

297

approach adds inputs including recovery efficiency, standby loss coefficient, and rated power to

298

provide a more detailed profile of the water heater used. The first method relies on water heater

299

EF, determined based on the amount of hot water produced per unit of fuel consumed over a typical

300

day, while the second method uses the WHAM equation (Lutz *et al.*, 1999); see Section 3.3 for

301

more detailed description of the latter. Because most homes in the United States use electric-

302

resistance water heaters or natural gas water heaters, saving estimates are confined to those energy

303

forms.

304 **3.1 Determination of the hot water energy savings equation**

305 For WaterSense, energy savings ($Q_{savings}$) have been calculated based on the amount of
306 water saved ($Vol_{WS_savings}$), the percentage of the saved volume that constitutes hot water
307 ($HW_{per_fitting}$), the ratio of water heaters using either natural gas or electricity to total residences with
308 plumbing systems, and the energy required to heat a unit volume of water (Q_{HW_vol}). (Section 2
309 describes the method used to estimate the percentage of hot water for showerheads and lavatory
310 faucets.) Equation 4 shows the EF/UEF-based method used to estimate water heating energy
311 savings from WaterSense-labeled lavatory fittings.

312
$$Q_{savings,WH_fuel} = Vol_{WS_savings} \times HW_{per_fitting} \times \frac{Houses_{WH_fuel}}{Houses_{total}} \times Q_{HW_vol,fuel} \quad \text{Equation 4}$$

313
314 Where:

- 315 $Q_{savings, WH_fuel}$ = heating energy savings (from electricity or natural gas water heater) from
316 WaterSense lavatory faucets or showerheads, kWh/year,
317 $Vol_{WS_savings}$ = total lavatory faucet or showerhead water savings from WaterSense lavatory
318 faucets or showerheads, L/year (gal/year),
319 $HW_{per_fitting}$ = percentage of water use that is hot water (see Section 2 for calculation),
320 WH_fuel = fuel type of water heater used, electric or natural gas,
321 $Houses_{WH_fuel}$ = number of households using electric or gas storage water heaters (from AHS
322 data),
323 $Houses_{total}$ = number of households with electric or gas water heaters (from AHS data), and,
324 $Q_{HW_vol,fuel}$ = heating energy (electricity or natural gas) required per unit of water volume
325 with ambient temperature, kWh/L (kWh/gal).

326 Note that the “total number of households” denominator ($Houses_{total}$) ideally should include
327 households using fuel types other than natural gas or electricity for their storage water heaters
328 and other water heater types. Insufficient data exist, so the authors made the conservative

329 assumption that the water heating energy consumption for these water heaters is similar to that of
330 electric and natural gas ones; the impact on water heating energy savings estimates should be
331 minor.

332 **3.2 Estimating energy savings per unit volume of heated water based on EF/UEF**

333 The energy required per unit volume of water ($Q_{HW_vol,fuel}$) is the key input to estimate the
334 energy saved by WaterSense showers and lavatory faucets shown in Equation 4. This section
335 describes EPA's WaterSense program EF/UEF-based approach for calculating $Q_{HW_vol,fuel}$.

336 To estimate the energy savings per unit volume of hot water, since 2006 EPA's WaterSense
337 program has used either EF (EPCA, 1975) or assumptions for overall efficiency (based on the most
338 recent estimates available from U.S. Department of Energy [DOE] water heater analyses). EF is
339 defined in the previous federal water heater test procedure (U.S. DOE, 2015); see Equation 5.

$$340 \quad EF = \frac{0.001 \times vol_{tp} \times den_{tp} \times C_{p,tp} \times (T_{tank,tp} - T_{in,tp})}{Q_{in} \times 3600} \quad \text{Equation 5}$$

341 Where:

342 EF = energy factor, unitless,

343 0.001 = m³ to Liter,

344 vol_{tp} = 243.4 L, volume of hot water drawn in 24 hours during the previous federal test
345 procedure (DOE 2015), L/day,

346 den_{tp} = density of water during the previous federal test procedure (DOE 2015), kg/m³,

347 $C_{p,tp}$ = specific heat of water during the previous federal test procedure (DOE 2015),
348 kJ/(kg × C) (Btu/lb × °F)),

349 $T_{tank,tp}$ = 57.2°C (135°F), the water heater setpoint value during the previous federal test
350 procedure (DOE 2015),

351 $T_{in,tp}$ = 14.4°C (58°F), the inlet water temperature during the previous test procedure
352 (DOE 2015),

353 3600 = kJ to kWh conversion, and

354 Q_{in} = total water heater energy consumption, kWh/day.

355 Based on Equation 4 and accounting for a range of EF values according to stock, energy
356 savings per unit volume of water for year y can be determined in Equation 6.

357
$$Q_{HW_{vol,fuel}} = \frac{0.001 \times den \times C_p \times (T_{tank} - T_{in})}{EF_{stock} \times 3600}$$
 Equation 6

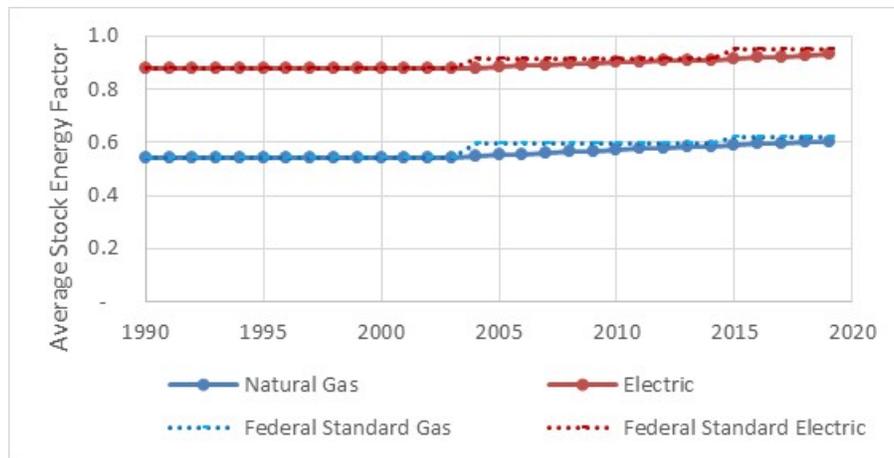
358 Where:

359 $Q_{HW_{vol,fuel}}$ = energy (electricity or natural gas) required per unit of water volume with ambient
360 temperature, kWh/L (kWh/gal), and

361 EF_{stock} = average energy factor of the stock.

362 Assuming a Weibull distribution for the retirement function and an average retirement age
363 of 13 years (DOE, 2014), EF minimum requirements from an ENERGY STAR market report
364 (DOE, 2010b), and water heater shipments from the Air-Conditioning, Heating, and Refrigeration
365 Institute (AHRI, 2019), the weighted average EF is calculated and used in the equation for water
366 heater energy use. See Figure 1.

367



368 **Figure 1: Average Shipment-Weighted Energy Factor per Stock Year (1990–2019) for Electric and**
369 **Natural Gas-fired Water Heaters**

370

371

372 **3.3 Estimating energy savings per unit volume of heated water using a WHAM-based**
373 **method**

374 This section describes a second approach to estimate the energy savings per unit volume
375 of water (presented in section 3.2) based on the WHAM. For demonstration purposes, the authors
376 have used recovery efficiency values from the 2010 DOE final rule technical supporting
377 documents (DOE, 2010c).

378 The WHAM is an equation for calculating the energy consumption of storage type
379 residential water heaters under different operating conditions (such as daily draw volume,
380 thermostat setpoint temperature, inlet water temperature, and ambient air temperature), different
381 water heater characteristics, and accounting separately for recovery and standby energy use.

382 The WHAM equation was developed under the assumption that the amount of energy
383 consumed by a storage water heater (Q_{in}) is equal to the sum of the energy consumed to heat the
384 water drawn from the water heater (Q_{recov}) plus the energy due to standby (Q_{stdby}), see Equation 7.
385 Standby in the WHAM equation is defined as the time when the water heater is not heating water
386 to recover from a draw, so the time when the burner is firing or the elements are energized to make
387 up for standby heat losses is included in the hours of standby.

388
$$Q_{in} = Q_{recov} + Q_{stdby} \qquad \text{Equation 7}$$

389 Where:

390 Q_{in} = total water heater energy consumption, kWh/day,

391 Q_{recov} = energy consumed to heat the water drawn from the water heater, kWh/day, and

392 Q_{stdby} = energy to make up for standby energy loss, kWh/day

393 The WHAM equation then uses federal water heater test procedure (U.S. DOE, 2015)
394 definitions and parameter inputs to estimate Q_{recov} and Q_{stdby} while continuing to use the energy
395 factor as defined in the prior DOE test procedure; see Equation 8 (U.S. DOE, 2009). The new

396 federal test procedure became effective July 13, 2015, changing the water heater efficiency metric
 397 from EF to uniform energy factor. Note that the WHAM equation has not been validated or
 398 modified to be used with the uniform energy factor (see Lutz, et al., 1999 for a complete discussion
 399 of the equation, including seasonal considerations).

$$400 \quad Q_{in} = \frac{Q_{out}}{RE} + H_{stdby} \times UA \times (T_{tank} - T_{amb}) \quad \text{Equation 8}$$

401 Where:

- 402 Q_{in} = total water heater energy consumption, kWh/day,
 403 Q_{out} = heat content of the water drawn from the water heater (subtracting for standby
 404 power heat content), kWh/day,
 405 = $vol \times den \times C_p \times (T_{tank} - T_{in})$,
 406 vol = volume of hot water drawn in 24 hours, L/day (gal/day),
 407 RE = recovery efficiency, %,
 408 H_{stdby} = hours of standby per day, h/day,
 409 = $24 - \frac{Q_{recov}}{P_{on}}$
 410 Q_{recov} = daily energy consumed to heat the water drawn from the water heater, J/day
 411 (Btu/day),
 412 P_{on} = rated input power, J/hr (Btu/hr),
 413 UA = standby heat loss coefficient, kW/°C (kW/°F),
 414 T_{tank} = water heater thermostat setpoint temperature, °C (°F),
 415 T_{amb} = ambient air temp around water heater, °C (°F).

416
 417 For the WaterSense model, it is unnecessary to determine the 24-hour energy consumption
 418 from water heating given that only the hot water savings from using more efficient WaterSense
 419 products is relevant to EPA. Instead, the authors calculate the energy consumption per unit water

420 volume ($Q_{HW_vol,fuel}$), which is then multiplied by the total hot water volume savings to determine
 421 the corresponding amounts of energy and carbon savings. Note that heat loss during a water heating
 422 event is considered minimal given the short time durations of the usage and therefore is not
 423 accounted for in this approach.

424 As the authors assumed that all WHAM equation parameters were the same with the
 425 exception of hot water volume, the resulting hot water energy savings calculation from using more-
 426 efficient WaterSense showerheads and lavatory faucets for year y ($Q_{savings,y}$) is shown in Equation
 427 9. Given the objective is to only characterize the fitting event energy savings, the expression
 428 related to the 24-hour standby energy use in Equation 8 cancels out because this parameter does
 429 not vary with changes in hot water use.

$$430 \quad Q_{savings,y} = \frac{0.001 \times vol_{savings,y} \times den \times Cp \times (T_{tank} - T_{in})}{RE_{stock,y} \times 3600} \times \left(1 - \frac{UA \times (T_{tank} - T_{amb})}{P_{on}} \right) \quad \text{Equation 9}$$

431 The subsequent expression for energy savings per unit water volume ($Q_{HWvol, fuel_WHAM,y}$),
 432 or $Q_{savings,y}$ divided by $vol_{savings,y}$, is described by Equation 10.

$$433 \quad Q_{HWvol, fuel_{WHAM},y} = \frac{0.001 \times den \times Cp \times (T_{tank} - T_{in})}{RE_{stock,y} \times 3600} \times \left(1 - \frac{UA \times (T_{tank} - T_{amb})}{P_{on,stock,y}} \right) \quad \text{Equation 10}$$

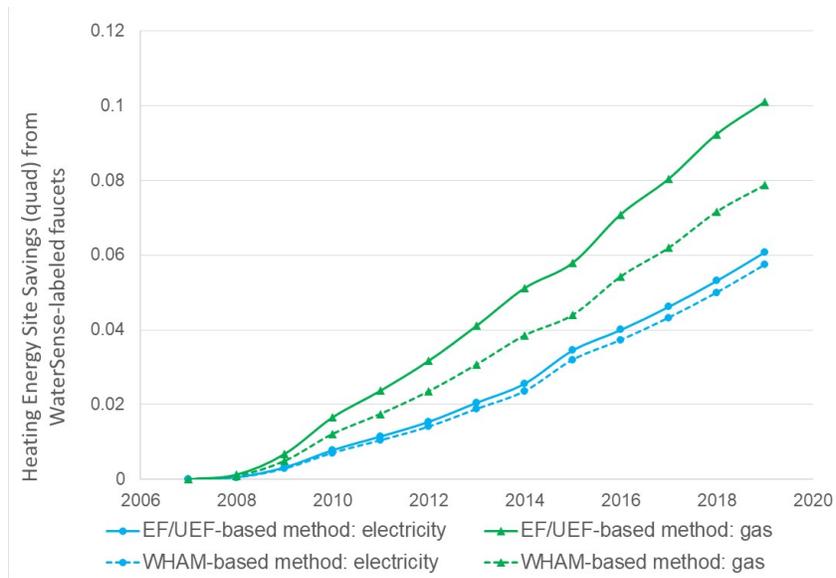
434 3.4 Site energy savings results

435
 436 Based on the 2019 inputs, the EF/UEF-based method of calculating energy savings per unit
 437 of hot water by lavatory fittings estimates 249.7 kJ/L (69.35Wh/L, 895.8 Btu/gal) for gas-fired
 438 water heaters and 44.78 Wh/L (169.5 Wh/gal) for electric storage water heaters. Estimates using
 439 the WHAM equation with the same inputs show 194.7 kJ/L (54.09 Wh/L, 698.7Btu/gal) and 42.24
 440 Wh/L (159.9 Wh/gal), respectively.

441 Figure 2 shows the evolution from 2007–2019 of site heating energy saving estimates
 442 resulting from the two methods for lavatory faucets and showerheads. The WHAM-based
 443 approach provides more conservative estimates for both electricity and gas savings compared to

444 the EF/UEF-based approach. The difference of saving estimates for gas-fired water heaters is
445 greater than the electric water heaters for three reasons: 1) the difference of magnitude of EF for
446 gas-fired and electric water heaters, 2) the introduction of RE in the WHAM approach, and 3) the
447 role EF and RE play in the two equations. The impact of introducing RE on the final energy savings
448 estimates (in the WHAM-based approach) is greater for gas-fired water heaters than for electric
449 ones, because the EF for electric water heater is close to 1 while the EF for gas-fired water heater
450 is close to $2/3$. The difference between RE and EF is greater for gas-fired water heaters (~ 0.15)
451 than for electric (~ 0.05), and in the EF/UEF-based method, the EF appears in the denominator
452 only, while in the WHAM equation, the RE has multiple appearances in both the denominator and
453 the numerator.

454



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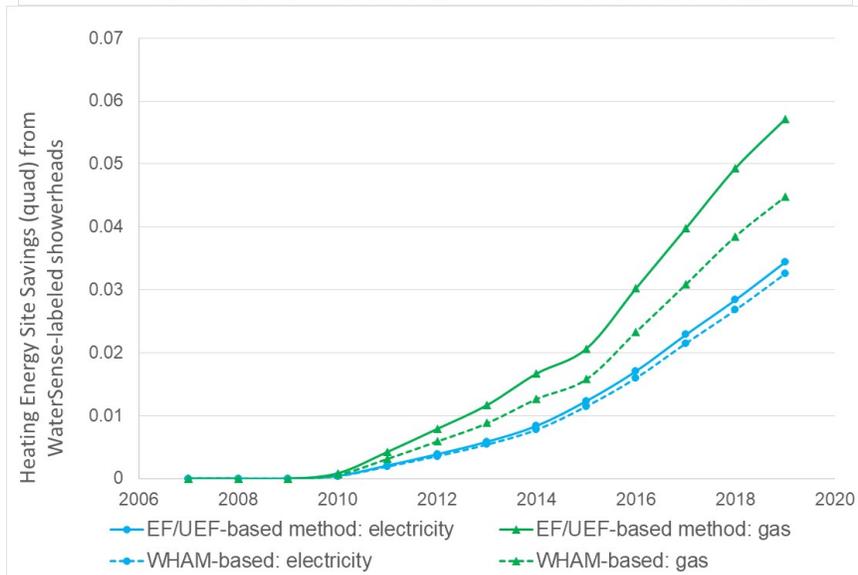


Figure 2: Heating energy site savings estimates (2007-2019) for WaterSense-labeled faucets (top) and showerheads (bottom) resulting from EF/UEF-based method and WHAM-based approach

460

4 DETERMINATION OF CARBON EMISSION SAVINGS

461

462

The U.S. EPA estimates site CO₂ emission savings attributable to WaterSense products.

463

The CO₂ emission savings are evaluated from the reduced load on water heaters used to bring water

464

to a warmer temperature at the showerhead or lavatory faucet and from the reduction in energy

465

from the treatment and delivery of drinking water, as well as from the treatment and distribution

466 of wastewater. Site emissions of CO₂ are estimated using emissions intensity factors from an EPA
 467 publication (Greenhouse Gases Equivalencies Calculator, 2019) based on a marginal analysis. The
 468 carbon emissions estimates account for the line losses for electricity,³ yet do not encompass the
 469 upstream component (full-fuel cycle factor).

470 The calculation to estimate CO₂ emissions reduction uses the estimates of embedded
 471 energy from annual water savings (*Vol_{WS_savings}*, *elec_{PW}*, and *elec_{WW}*) from the water and
 472 wastewater utility, energy from annual hot water savings (*Q_{savings}*) using the WHAM-based
 473 method, metric tons of CO₂ per kWh (*CO_{2_kWh}*), and metric tons of CO₂ per kilojoule (*CO_{2_kj}*).
 474 Equation 11 shows the calculation of carbon emissions reductions.

$$475 \quad Mt_{CO_2} = \left(\left(\left(Vol_{WS_{savings}} \times (elec_{PW} + elec_{WW}) \right) + Q_{savings_{elec}} \right) \times CO_{2_{kWh}} \right) + (Q_{savings_{gas}} \times CO_{2_{MJ}})$$

476 **Equation 11**

477 Where:

- 478 *Vol_{WS_savings}* = volume of water saved by WaterSense showerheads and lavatory faucets,
- 479 *elec_{PW}* = energy required to convey potable water, kWh/unit of water,
- 480 *elec_{WW}* = energy required to treat wastewater, kWh/unit of water,
- 481 *Q_{savings}* = energy savings from annual hot water savings (electricity and natural gas),
- 482 *CO_{2_kWh}* = metric tons of CO₂ per kWh,
- 483 *CO_{2_MJ}* = metric tons of CO₂ per MJ (per therm).

³ Because the distance between the point of use and point of generation for electricity is usually substantial, a reduction in kWh also results in a reduction in emissions from generation that would have had to cover the line losses. This explains why line losses were accounted for in the electricity CO₂ emission estimate. By contrast for natural gas, fuel is transported a long distance but energy generation occurs very close to the point of use. So while that's not to suggest that 100% of the natural gas put into a pipe is actually combusted, reductions in the demand for natural gas do not necessarily result in additional reduction of emissions. Therefore, no line loss was assumed in the corresponding carbon emission estimates.

484 In Table 4, the emission savings estimates from 2019 for lavatory fittings resulting from
485 the two approaches mentioned above are compared. The embedded energy savings (potable and
486 wastewater) are equal for the two methods given the same amount of water savings (Table 4 Part
487 1). The second and third parts of the table show energy savings from electric and gas water heaters
488 respectively, while the fourth part is a sum of electricity savings for both embedded and water
489 heater electricity and gas savings for water heater energy. The last two parts show the
490 corresponding carbon dioxide savings estimates. Critical distinctions between the two calculation
491 methods can be found in Part 2 and Part 3 of the table. Heating energy savings estimates are larger
492 for gas water heaters compared to heating energy savings estimates for electric water heaters
493 because of the role of EF and RE in the calculations (See Section 3.4.). Estimate differences in
494 Parts 4 through 6 are rooted in Parts 2 and Part 3, and differ according to the addition of embedded
495 electricity savings or emissions multipliers.

Table 4: Summary of Carbon Emissions Savings Results for 2019

Part 1: Embedded annual electricity savings^a (quad)			
	EF/UEF-based method	WHAM-based method	
Faucet		0.0056	
Showerhead		0.0029	
Part 2: Heating energy savings from electric water heater (quad)			
	EF/UEF-based method	WHAM-based method	% difference
Faucet	0.0608	0.0574	5.6%
Showerhead	0.0345	0.0326	5.5%
Part 3: Heating energy savings from gas water heater (quad)			
	EF/UEF-based method	WHAM-based method	% difference
Faucet	0.1009	0.0787	22.0%
Showerhead	0.0572	0.0448	21.7%
Part 4: Total energy savings from heating energy and embedded electricity savings (quad)			
	EF/UEF-based method	WHAM-based method	% difference
Faucet	0.17	0.14	15.3%
Showerhead	0.09	0.08	15.1%
Part 5: Emission reduction from heating energy savings (million metric tons)			
	EF/UEF-based method	WHAM-based method	% difference
Faucet	18.0	16.1	10.5%
Showerhead	10.2	9.1	10.2%
Part 6: Emission reduction from all energy saved (million metric tons)			
	EF/UEF-based method	WHAM-based method	% difference
Faucet	19.1	17.2	9.9%
Showerhead	10.8	9.7	9.7%

497 ^a Energy that would have been required to convey potable water and treat wastewater for the water saved by
 498 WaterSense products.
 499

500

5 DISCUSSION

501 This study sought to establish a nationally representative estimate of the mix of hot and
 502 cold water for two WaterSense-labeled residential products that use hot water: showerheads and
 503 lavatory faucets. Analysis including 2015 RECS microdata improves upon values previously used
 504 in the EPA WaterSense model, which had relied on regional studies with small sample sizes. Use
 505 of RECS microdata, with its large sample size, enables a more accurate estimation of hot water
 506 percentage by incorporating temperature differences across the nation, establishing a nationally
 507 representative picture of the mix of hot and cold water usage for each product. Further, the
 508 proximity of these results to those found through two regional studies corroborate these findings.

509 The EPA WaterSense program saves not only water by reducing per-unit consumption
510 from individual fittings, but also energy from avoided water heating associated with that use. This
511 study proposed an alternative to the EF/UEF-based approach, which relied solely on EF, by using
512 the modified WHAM-based approach with both EF and RE to account for hot water energy savings
513 per unit volume. The modified WHAM-based approach updates the energy content calculation to
514 include only heated water savings volumes and exclude standby energy use, which leads to a more
515 conservative estimate of the savings that may occur in practice.

516 Figure 2 shows the estimated hot water savings based on the EF approach in comparison
517 to the modified WHAM equation. Employing the WHAM-based approach reduces estimated
518 energy savings per unit volume by 22 percent for gas-fired and 5.7 percent for electric water
519 heaters. These revised estimates are more conservative and were calculated using a more detailed
520 profile of the water heaters used. In the case that more granular annual average water heater profile
521 data become available, the WHAM-based approach would provide more conservative and
522 technically accurate estimates of the heating energy saved plus the corresponding emissions
523 reduction. Importantly, the refinement of the hot water percentage and savings saw changes to the
524 carbon emissions savings associated with the efficiency improvements of the WaterSense
525 program.

526 In this study, the authors not only solicited more up-to-date usage information to inform
527 the total water consumption that directly affects hot water consumption estimates, but also
528 reviewed the assumptions and the core methodology for assessing the heating energy required per
529 unit of hot water. Given water efficiency improvements achieved over time due to DOE appliance
530 standards and labeling programs, frequent review of the estimation tool is necessary to achieve
531 more realistic and robust estimates of energy consumption outcomes resulting from potential

532 policy scenarios. The workflow presented here could easily be adapted for heating energy usage
533 estimations of other appliances and fixtures as a decision guide or usage monitoring tool for
534 various stakeholders, such as water utilities, water conservation programs, appliance standards,
535 and government regulation programs.

536

537

6 CONCLUSION AND FUTURE WORK

538 This paper discusses refinements to two inputs in the calculation of both heating energy
539 savings and carbon emissions reduction attributable to hot water-using residential products of the
540 EPA WaterSense program. The first input discussed is the hot water percentage of lavatory fitting
541 flow volume, which can show variability in temperature due to geographic location. The second
542 input is the calculation of the energy content of lavatory fitting hot water. Based on the literature
543 review conducted, (1) a nationally representative publicly available dataset can closely
544 approximate regional field study values for hot water percentages for lavatory fittings. While
545 increased precision can be achieved with the WHAM energy use equation, (2) reasonably
546 approximate values can be obtained using shipment-weighted energy factors when more precise
547 data are not available. (3) The approach described in this paper is generic and can be used to
548 quantify potential water heating energy savings as well as the carbon emission reductions for
549 similar water conservation programs.

550 As new data become available, the WaterSense models' structure permits updates to these
551 inputs to reflect the most up-to-date assessment of energy savings possible. The method used to
552 estimate the percentage mix of hot water usage for both lavatory faucets and showerheads can be
553 updated with RECS 2020 data once available. Further, the WHAM equation uses the federal water
554 heater test procedure definitions and input parameters to establish several key inputs. This test

555 procedure undergoes periodic updates and revisions. As such, future assessments of emissions
556 savings from the reduction in water heating energy use for WaterSense-labeled products could use
557 the most recent test procedure and be updated accordingly. Additional improvements to further
558 refine the CO₂ emissions savings estimates include expanding this model to incorporate upstream
559 energy savings from energy utilities. The estimate could also include other emissions savings such
560 as Hg, NO_x, SO₂, CH₄, and N₂O by using their associated emission factors, and projections of
561 future emission savings could be refined by using a forecast of these factors.

562

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564

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567

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